

EFFECTS OF THE ADDITION OF METAL OXIDES ON THE REDUCTION OF  
NITRIC OXIDE WITH HYDROGEN ON Pt/Al<sub>2</sub>O<sub>3</sub> CATALYST

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The selectivity to NH<sub>3</sub> in the NO-H<sub>2</sub> reaction on Pt/Al<sub>2</sub>O<sub>3</sub> has been markedly decreased by the addition of metal oxides. This effect has been found to be brought by the hydrogen spillover from Pt to metal oxides, and by a successive reaction of NH<sub>3</sub> ( the NO-NH<sub>3</sub> reaction ) as an intermediate of the NO-H<sub>2</sub> reaction.

Attention is focused on the three-way catalyst system for the control of automotive exhaust emissions. This technique brings about the simultaneous removal of nitric oxide, carbon monoxide, and hydrocarbons in a single bed of supported metal catalyst by the use of an oxygen sensor in order to hold the air/fuel ratio at the stoichiometric point.<sup>1)</sup> However, unavoidable dynamic fluctuation of the air/fuel ratio around the stoichiometric point prevents a successful operation of the technique. In order to solve this problem, it is desired to give an oxygen storage ability to a supported metal catalyst.<sup>2)</sup> In this work, the effects of the addition of metal oxides on the reduction of NO by H<sub>2</sub> on Pt/Al<sub>2</sub>O<sub>3</sub> catalyst have been investigated at the reducing inlet composition, since reactions involved in the real three-way catalyst consist of many complex ones and, among those, the reaction of NO with H<sub>2</sub> ( one of main reducing components at the reducing inlet composition of exhaust gas ) is considered to be one of the most important reactions.

Method of preparation of metal oxides ( V<sub>2</sub>O<sub>5</sub>, MoO<sub>3</sub>, WO<sub>3</sub>, and SnO<sub>2</sub> ) was described previously.<sup>3)</sup> Pt/Al<sub>2</sub>O<sub>3</sub> ( Pt loading of 0.5 wt % ) was purchased from Nippon Engelhard. Pt/Al<sub>2</sub>O<sub>3</sub>-metal oxide mechanical mixtures were prepared by mixing powder of equal amounts of both components in an agate mortar for 20 min without water ( this is hereafter denoted as Mixing ), or by shaking particles of both components ( 28 - 48 mesh ) ( this is denoted as Shaking ). Experiments were carried out by an ordinary pulse apparatus. Helium or argon as carrier gas was purified with the titanium metal sponge heated at 750 °C, and a Molecular Sieve trap. The reaction temperature was 297 °C. Pulse size was 18.22 cm<sup>3</sup> and the inlet concentration of NO in pulse was 2.3 %. Carrier gas flow rate was 87 cm<sup>3</sup>/min.

The metal oxides employed in this work were all found to be inactive for the NO-H<sub>2</sub> reaction, and not to be treated by H<sub>2</sub>. Figure 1 shows the results of the NO-H<sub>2</sub> reaction on both Pt/Al<sub>2</sub>O<sub>3</sub> and Pt/Al<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> (Mixing). On Pt/Al<sub>2</sub>O<sub>3</sub>, when the ratio of the inlet concentration of H<sub>2</sub> ( C<sub>H<sub>2</sub></sub><sup>o</sup> ) to that of NO ( C<sub>NO</sub><sup>o</sup> ) was larger than unity, i.e. at the reducing inlet composition, NH<sub>3</sub> was produced as a product, while NO was completely

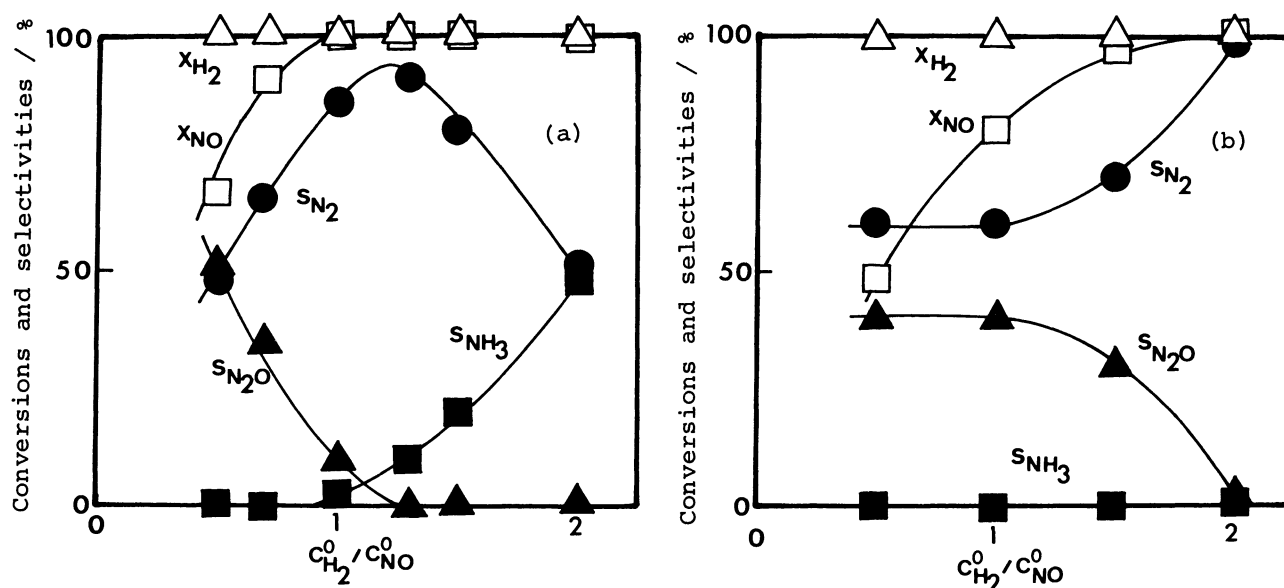


Figure 1. Conversions and selectivities in the NO-H<sub>2</sub> reaction on Pt/Al<sub>2</sub>O<sub>3</sub> and Pt/Al<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> (Mixing).  
(a), Pt/Al<sub>2</sub>O<sub>3</sub> = 0.1 g; (b), Pt/Al<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> (Mixing) = 0.2 g.

removed. As  $C_{H_2}^0/C_{NO}^0$  increased, the selectivity to NH<sub>3</sub> ( $S_{NH_3}$ ) increased and attained as high as 50 % at  $C_{H_2}^0/C_{NO}^0 = 2.0$ . These behaviors of each component are similar to those in the NO-H<sub>2</sub>-O<sub>2</sub> reaction near the stoichiometric point.<sup>4)</sup> On the other hand, on Pt/Al<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> (Mixing), NH<sub>3</sub> was not produced in the whole range of the inlet composition indicated in Fig. 1, while the conversion of NO ( $X_{NO}$ ) decreased slightly. It is therefore evident that the addition of V<sub>2</sub>O<sub>5</sub> to Pt/Al<sub>2</sub>O<sub>3</sub> is an effective way to control the formation of NH<sub>3</sub> in the "rich" region, i.e.  $C_{H_2}^0/C_{NO}^0 > 1$ .

In order to study the mechanism of the effects of metal oxides on the reaction, following experiments were made: In Table 1, results of both the reaction of H<sub>2</sub> with mixing catalysts and the NO-H<sub>2</sub> reaction at the reducing inlet composition ( $C_{H_2}^0/C_{NO}^0 = 2.0$ ) are shown for various states of mixing. Since the enhanced rate of the reduction of a metal oxide by H<sub>2</sub> in a precious metal-metal oxide mixture is well documented in terms of the hydrogen spillover,<sup>5)</sup> the conversion of H<sub>2</sub> ( $X_{H_2}$ ) in the reaction of H<sub>2</sub> with

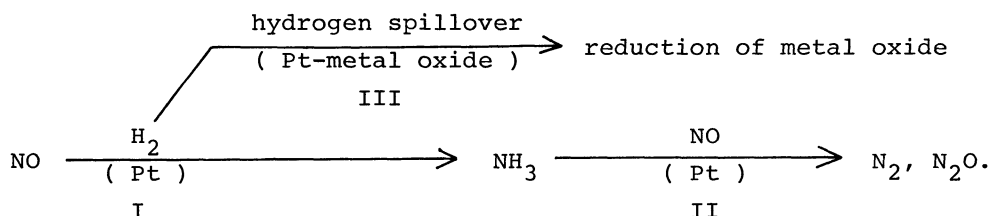
Table 1. Relationship between the reaction of H<sub>2</sub> with mixtures and the NO-H<sub>2</sub> reaction

Catalyst	The reaction of H <sub>2</sub> with catalyst <sup>a)</sup>	The NO-H <sub>2</sub> reaction <sup>b)</sup>			
	$X_{H_2}$ (%)	$X_{NO}$ (%)	$S_{NH_3}$ (%)	$S_{N_2}$ (%)	$S_{N_2O}$ (%)
V <sub>2</sub> O <sub>5</sub> (0.1 g)	0	0	-	-	-
Pt/Al <sub>2</sub> O <sub>3</sub> (0.1 g)	0	100	49	51	0
Pt/Al <sub>2</sub> O <sub>3</sub> -V <sub>2</sub> O <sub>5</sub> (Shaking) (0.2 g)	0	100	46	54	0
Pt/Al <sub>2</sub> O <sub>3</sub> -V <sub>2</sub> O <sub>5</sub> (Mixing) (0.2 g)	70	100	0	97	3

a), Conc. of H<sub>2</sub> in pulse = 3.7 %; b), Conc. of NO in pulse = 2.3 % ( $C_{H_2}^0/C_{NO}^0 = 2.0$ ).

the mixing catalysts can be used as a measure of the extent of the hydrogen spillover. From Table 1, it is noted that the hydrogen spillover did not occur in Pt/Al<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> (Shaking), whereas, it did occur in Pt/Al<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> (Mixing). In conformity with the behaviors of the hydrogen spillover,  $S_{\text{NH}_3}$  in the NO-H<sub>2</sub> reaction on Pt/Al<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> (Shaking) was almost the same as that on Pt/Al<sub>2</sub>O<sub>3</sub>, while that on Pt/Al<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> (Mixing) was completely decreased. Furthermore, as shown in Fig. 2,  $S_{\text{NH}_3}$  in the NO-H<sub>2</sub> reaction on Pt/Al<sub>2</sub>O<sub>3</sub>-metal oxide (V<sub>2</sub>O<sub>5</sub>, MoO<sub>3</sub>, WO<sub>3</sub>, or SnO<sub>2</sub>) (Mixing) decreased with increasing  $X_{\text{H}_2}$  in the reaction of H<sub>2</sub> with the mixing catalysts, that is, the extent of the hydrogen spillover. These results indicate that the extent of the hydrogen spillover from Pt to metal oxides influences the selectivity to NH<sub>3</sub> in the NO-H<sub>2</sub> reaction on Pt in Pt/Al<sub>2</sub>O<sub>3</sub>-metal oxide mixing catalysts.

Figure 3 shows results of the NO-H<sub>2</sub> reaction on different amounts of catalyst for both Pt/Al<sub>2</sub>O<sub>3</sub> and Pt/Al<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> (Mixing). The data can be explained in terms of the following scheme:



According to this scheme, NO is first reduced by H<sub>2</sub> to NH<sub>3</sub> (Step I) on Pt and NH<sub>3</sub> then reacts with NO (Step II; the NO-NH<sub>3</sub> reaction) on Pt to form N<sub>2</sub> and N<sub>2</sub>O. This is in accordance with experiments, since the selectivity of the reaction to NH<sub>3</sub> ( $S_{\text{NH}_3}$ ) increases with decreasing catalyst weight (Fig. 3(a)). In the presence of metal oxide, Step III (that is, hydrogen spillover) takes place in addition of Steps I and II, and Step I and Step III proceed competitively. Near the inlet of catalyst bed ( $W < 0.01$  g), as shown in Fig. 3(b), the formation of NH<sub>3</sub> by Step I occurs readily and H<sub>2</sub> is markedly removed by both Steps I and III. At the following part of catalyst bed ( $W > 0.01$  g), Steps I and III scarcely take place because of the considerable decrease of H<sub>2</sub> concentration and the reaction of NO with NH<sub>3</sub> (Step II) causes the complete removal of both NO and NH<sub>3</sub>. In other words, when Pt/Al<sub>2</sub>O<sub>3</sub> is mechanically mixed with the metal oxide, the hydrogen spillover (Step III) proceeds as fast as the formation of NH<sub>3</sub> (Step I). This brings about a significant decrease of the selectivity to NH<sub>3</sub>, while the conversion of NO is little decreased.

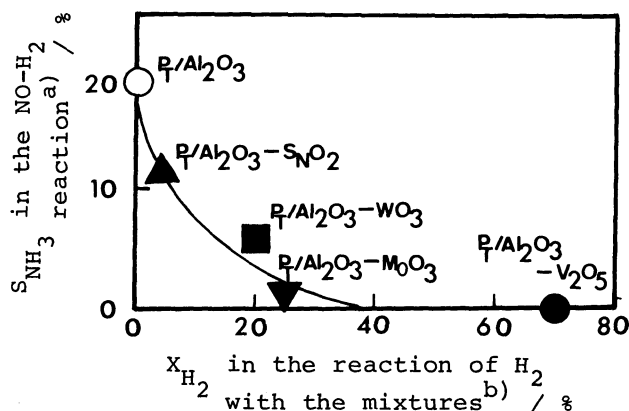


Figure 2. Relationship between  $X_{\text{H}_2}$  in the reaction of H<sub>2</sub> with Pt/Al<sub>2</sub>O<sub>3</sub>-metal oxide (Mixing) and  $S_{\text{NH}_3}$  in the NO-H<sub>2</sub> reaction. Pt/Al<sub>2</sub>O<sub>3</sub> = 0.1 g. Pt/Al<sub>2</sub>O<sub>3</sub>-metal oxide (Mixing) = 0.2 g. a),  $C_{\text{H}_2}^0 / C_{\text{NO}}^0 = 1.5$ . b), Concentration of H<sub>2</sub> in pulse = 3.7 %.

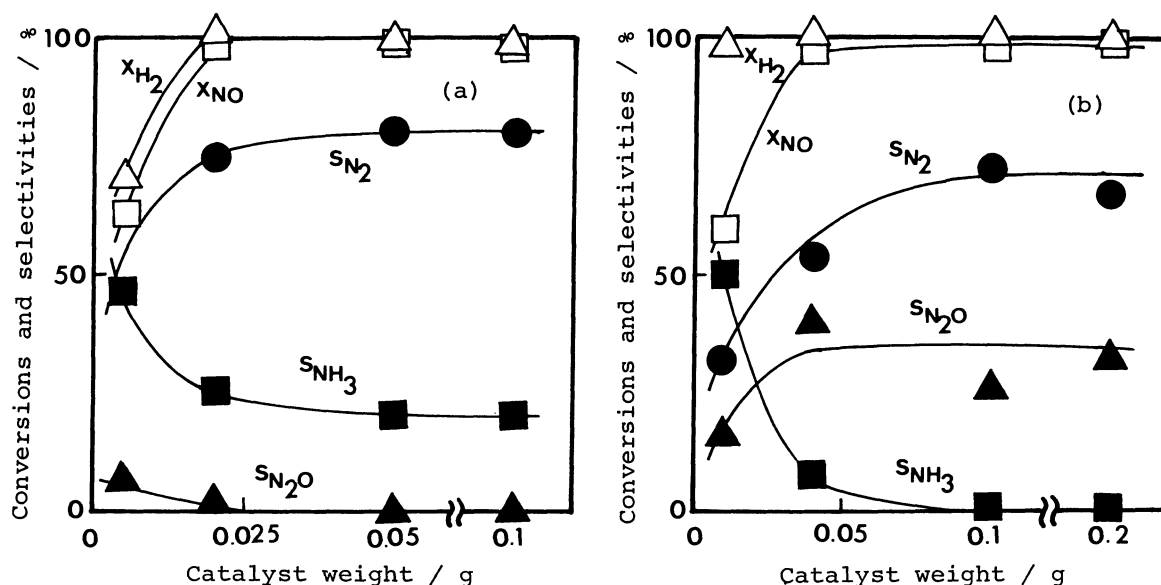


Figure 3. Conversions and selectivities in the NO-H<sub>2</sub> reaction on Pt/Al<sub>2</sub>O<sub>3</sub> and Pt/Al<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> (Mixing).  
 (a), Pt/Al<sub>2</sub>O<sub>3</sub>; (b), Pt/Al<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>5</sub> (Mixing).  
 $C_{H_2}^0/C_{NO}^0 = 1.5$ .

As mentioned above, the metal oxide in Pt/Al<sub>2</sub>O<sub>3</sub>-metal oxide (Mixing) is reduced at the reducing inlet composition to treat NO without the formation of NH<sub>3</sub> at the outlet of reactor. The reduced metal oxide in the mixing catalyst was then confirmed to be reoxidized by O<sub>2</sub> pulse. Similarly, the reduced metal oxide is considered to be readily oxidized by O<sub>2</sub> in the oxidizing composition of exhaust gas.<sup>2)</sup> In other words, the metal oxide in the mixing catalyst is reduced to remove excess H<sub>2</sub> by hydrogen spillover at the reducing inlet composition and is reoxidized to remove excess O<sub>2</sub> at the oxidizing inlet composition. Therefore, the oxidation state of the metal oxide in the Pt/Al<sub>2</sub>O<sub>3</sub>-metal oxide mixing catalyst is expected to be maintained after the whole cycle of the dynamic fluctuation of the inlet gas between reducing and oxidizing compositions. This means that the whole process can proceed catalytically with the redox cycle of the metal oxide according to the dynamic fluctuation of the composition of the inlet gas, suggesting that the addition of the metal oxide to supported metal catalyst is a promising way to deal with the dynamic fluctuation of the composition of exhaust gas.

#### REFERENCES

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